

Fracture resistance of palatal cusps defective premolars restored with polyethylene fiber and composite resin

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The aim of the study was to compare the fracture resistance of the palatal cusps of defective and endodontically treated premolars after restoration with various restorative techniques. Fifty premolars were assigned to five groups. The first group comprised intact teeth as control (G1), while the other experimental groups (G2, G3, G4 and G5) comprised endodontically-treated teeth, whose palatal cusps were cut and reduced the buccal cusps by 2 mm. G2, composite resin onlay with buccal cusp coverage (CR). G3, CR and fiber post. G4, CR and polyethylene fiber. G5, CR, fiber post and polyethylene fiber. Fracture resistance was tested. The data were recorded in Newton and submitted to ANOVA and Tukey *post hoc* tests. Statistically significant difference was found between the mean fracture resistances of the groups. Polyethylene fiber reinforced composite restorations strengthened the fracture resistance of palatal cusps defective and endodontically treated premolars.

Keywords: Composite resin, Ribbond, Cusp coverage, Fracture mechanics

INTRODUCTION

Compared to the intact teeth, endodontically treated teeth are considered increasingly susceptible to fracture as they have reduced lower water content, deeper cavities and less dentin^{1,2}. The anatomical shape of the maxillary premolar facilitates the fracture of cusps under occlusal loads³. Fractures of the teeth palatal cusps command special attention and consideration during the decision-making process of their restorative treatment options².

The remaining structure can be restored with composite, rather than post-core techniques⁴. These attributes of the elastic modulus of composites approximate those of the tooth structure, such that less force will be exerted on the tooth/restoration interface and the stress generated by the occlusal force will be distributed along the tooth⁵. For these reasons, it is possible to restore the premolar without palatal cusp with resin composite. The premolar without palatal cusp can be treated as if only one cavity wall remains, and a post should be inserted⁶. Fiber posts with a modulus of elasticity similar to dentin, when subjected to a compressive load, can better distribute forces along the long axis of the post, which may decrease the probability of root dentin fracture⁷. However, some studies revealed that endodontically treated maxillary premolars without fiber posts exhibited similar fracture resistance to those with a post^{5,8}.

Several authors recommend cusp coverage to restore weak posterior teeth⁹. Actually, some clinical trials achieved promising results with this method for the restoration of severally destroyed posterior

teeth^{10,11}. However, little data are available about the effect of composite coverage on the fracture resistance of premolar teeth when the palatal cusps are defective.

In recent years, there have been many studies on fiber-reinforced composite (FRC)^{11,12}, and has become a promising alternative for restorative dentistry. The leno wave ultra-high modulus (LWUHM) polyethylene fiber (Ribbond) has provided the opportunity to improve the performance of existing materials. Ribbond is a reinforced ribbon whose special fiber network enables the force distribution along the fiber¹³, and provides adequate mechanical properties^{12,13}. FRC has been used for orthodontic applications and to fabricate single crowns, full and partial coverage-fixed partial dentures, and periodontal splints¹⁴.

With the development of new materials and technology, new approaches can be implemented when faced with some of these cases to complement traditional methods. Only some studies have investigated the effects of fiber post, direct composite resin or FRC-restored on root-filled treated premolars with MOD cavity^{15,16}. Furthermore, few studies have evaluated the fracture strength of teeth restored with fiber post combined with a fiber ribbon.

The aim of the study was to test the fracture resistance and fracture patterns of endodontically-treated maxillary premolar teeth with fractured palatal cusps restored by different approaches. The null hypothesis tested was that there is no difference between the different restoration methods used to restore these teeth.

Color figures can be viewed in the online issue, which is available at J-STAGE.

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MATERIALS AND METHODS

Fifty sound, single-rooted, human maxillary premolars, with double canals, freshly-extracted for orthodontic reasons were collected in our study. The debris and soft tissue were carefully removed using a hand scaler. The teeth, free of root canal resorptions, were selected and examined at 10× magnification using a stereomicroscope (Carl Zeiss, Oberkochen, Germany), and the teeth with cracks were excluded from the study. Next, teeth were stored in a 0.1% thymol solution at room temperature and used within 3 months. Then, the teeth were classified and randomly distributed, according to the size of the teeth and the tooth root length, into five groups ($n=10$). The teeth were prepared as follows.

All teeth except those in the G1 were subjected to root canal treatment. Standardized endodontic access cavities were prepared using a water-cooled diamond bur in a high-speed handpiece. A size 15 K-file (Mani, Tochigi, Japan) was inserted into each canal until it could be seen at the apical foramen. The working length was set at 1 mm short of the apical foramen. The root canals were prepared using the ProTaper system (Dentsply Maillefer, Ballaigues, Switzerland) following the manufacturer's guidelines, from SX to F3 at the working length. The canals were irrigated with 1% sodium solution and dried with paper points, and then obturated with gutta-percha (Dentsply Maillefer) and an AH Plus sealer (Dentsply Maillefer) using the cold lateral condensation technique. Subsequently, the access cavities were filled with glass ionomer cement (GIC) (Fuji IX GP, GC, Tokyo, Japan).

After 24 h, the GIC was removed, followed by the removal of the palatal cusps of the experimental groups teeth at the central fissure of the occlusal surface and the gingival wall parallel to cemento-enamel junction (CEJ) using a diamond fissure bur. The buccal cusps were reduced 2 mm. The specimens were subsequently restored with different techniques. The restorative steps for teeth of all the groups are as follows:

In the first group, intact teeth were used as controls.

In the second group, teeth were restored using only composite resin onlay with buccal cusp coverage. The adhesive surfaces were etched with 37% phosphoric acid (3M ESPE, St. Paul, MN, USA) for 20 s, rinsed with a water spray for 10 s and gently air dried, leaving the surfaces moist. The surfaces were treated with an adhesive bonding system (Single Bond, 3M ESPE); adhesives were applied in two layers and light-cured for 10 s with a light-curing unit (VIP Junior, Bisco, Schaumburg, IL, USA) at 600 mW/cm² light intensity. After fixation of the matrix band with a retainer, it was restored with a B2-shaded composite resin (Filtek P60, 3M ESPE) using the incremental technique (restoring first the proximal and lingual wall). The composite resin was applied in 1.5–2 mm increments and every layer was cured for 20 s from the occlusal surface. The last layer was light activated for 40 s. Additionally, the reduced buccal cusps were covered to a thickness of 2

mm with the composite resin. One operator performed all the preparations and restorations.

In the third group, the teeth were restored with glass fiber posts and composite resin. A select universal drill was used to remove 2/3 of the filling material from the root canal, then the post system drill (RelyX Fiber Post drill 2#) (3M ESPE) was used to widen and shape the root canal following the instructions provided by the manufacturer. Following the post space preparations, the canals were flushed with 2 mL of 5.25% NaOCl and 2 mL of saline solution. The root canal walls were gently dried, then the resin cements (Rely X Unicem, 3M ESPE) were delivered into the post space. Fiber posts were cleaned with 95% ethyl alcohol, air-dried, and then seated to canal spaces after the resin cements were dispensed into the post space. Next, using the moderate pressure to hold the post in position for 10 s, the excess of cement was removed with a brush and the material was light-activated for 40 s from the occlusal face to apical foramen. After cementation, the remaining post length was cut off and the teeth were restored using a procedure similar to that used for the G1.

In the fourth group, the teeth were restored with Ribbond and composite resin as illustrated in Fig. 1. The teeth were restored using the same dentine bonding system and composite resin as those used in G3. Before recovering the reduced buccal cusps and leaving 2 mm palatal cusps unrestored, the occlusal surface of the teeth between the cusp tips, a 3-mm wide layer of polyethylene ribbon fiber (Ribbond-THM, Ribbond, Seattle, WA, USA) was laid from buccal to lingual direction. The ribbon fiber was then cut, followed by wetting with adhesive resin (Single bond, 3M ESPE), and blotting off the excess with a lint free gauze. The same adhesive system was applied to the cavity walls and cured. Subsequently, a thin 0.5 mm layer of flowable composite resin (Filtek Supreme Ultra Flowable, 3M ESPE) was applied to the place where ribbon fiber was seated and then uncured. Next, the wetted ribbon fiber was pressed through the flowable composite as close to the cusp as possible and cured for

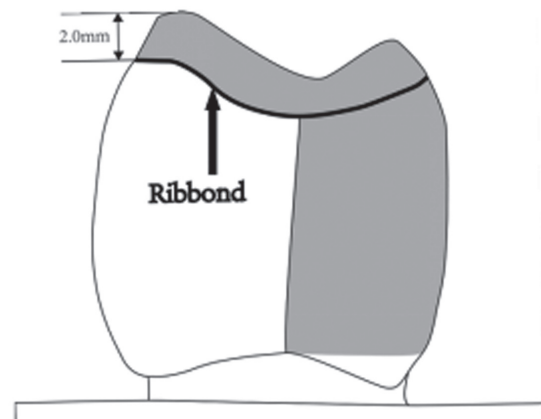


Fig. 1 Appearance of the teeth restored with Ribbond and composite resin (G4).

40 s. Restoration was recovered with composite, in the same manner as in G2.

In the fifth group, the teeth were restored with glass fiber posts, Ribbond and composite resin. The teeth received a post in a similar manner as described for G3 and were filled with Ribbond and composite resin in a similar way as described for G4.

All the restored and intact teeth were stored at 37°C in 100% humidity for 24 h and thermocycled for 2,000 cycles at 5 and 55°C with a 30 s dwell time and 5 s for transfer. Subsequently, all the teeth roots were vertically embedded in self-curing acrylic resin to a level of 1.0 mm apical to the CEJ and applied about 0.3 mm thick silicone paste between the roots and acrylic resin to simulate the periodontal ligament.

Static fracture resistance testing was performed with a universal testing machine (Instron, Canton, MA, USA). A vertical compression load test was conducted at a constant crosshead speed of 0.5 mm/min. The force was applied by a 4-mm-diameter metal bar, the bar was positioned parallel to the long axes of the teeth, toward the occlusal central fossae of the teeth and contacting the buccal and lingual cusps. The force necessary to fracture the restoration was recorded in Newtons (N). One-way analysis of variance (ANOVA) test followed by Tukey *post hoc* test were carried out to compare the differences between the five groups at a significance level of 0.05.

Finally, the fractured teeth were examined under 10× magnification to determine the fracture modes. To evaluate whether the fracture mode was favorable (fractures ending less than 1 mm below the CEJ) or unfavorable (fractures ending more than 1 mm below the CEJ), a comparison of the failure modes of the specimens was performed using the Chi-square test. All statistical analyses were carried out in SPSS11.0 (SPSS, Chicago, IL, USA).

RESULTS

The fracture resistance mean and standard deviation values of all samples are presented in Table 1. According to the assessment of the difference between the groups by the ANOVA test the differences between the mean fracture resistance of the groups were statistically significant ($F_{4, 50}=6.39, p<0.001$). Therefore our null hypothesis was rejected.

Additionally, the Tukey *post hoc* test revealed no significant difference between the fracture resistance of the G1, G4 and G5. The G1 was more resistant to fracture than G2 and G3 ($p<0.05$). In addition, G2, G3 and G4 were found to be statistically similar.

The favorable and unfavorable fractures percentage of the teeth are displayed in Figs. 2 and 3. Favorable fractures were predominant in all specimens (80 to 90%) except in G2 and G3. Specifically, in G2, the favorable

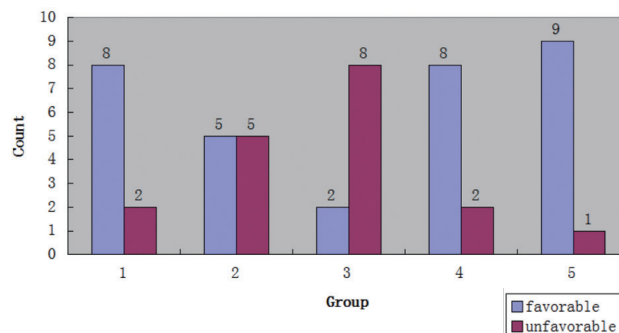


Fig. 2 The number of favorable and unfavorable fracture modes.

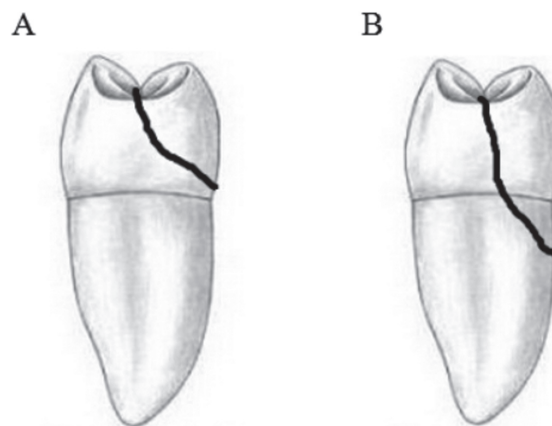


Fig. 3 Mode pattern of 2 types of fracture modes of samples: (A) favorable fracture; (B) unfavorable fracture.

Table 1 Comparison of the fracture strengths between restoration methods

Group (n)	Mean (SD)	Subgroups ($\alpha=0.05$)	
1 (10)	1,333.9 (461.1)	A	—
2 (10)	840.6 (499.9)	—	B
3 (10)	679.1 (349.0)	—	B
4 (10)	1,036.8 (331.8)	A	B
5 (10)	1,410.0 (266.8)	A	—

Analysis of variance (ANOVA) test and Tukey *post hoc* test

and unfavorable fracture modes were approximately equal, whereas in G3 most of the fractures (80%) were unfavorable.

DISCUSSION

It has been demonstrated that normal endodontic access in a healthy tooth has a mere effect on the fracture strength of the tooth¹⁷⁻¹⁹. Steele and Johnson reported that the mean fracture strength for unrestored teeth with MOD preparation was 50% weaker than that of unaltered premolar teeth¹⁸. Additionally, an MOD cavity preparation in a root-filled tooth may cause cuspal fracture^{15,16}. As the palatal cusps of teeth fracture, the severely destroyed teeth is usually recommended to be restored by post-core techniques. Metal post as the most commonly used material in clinical practice, but post dislocation and root fracture are the main reasons of failure²⁰. Meanwhile, several attempts have been made to improve the fracture resistance of endodontically treated teeth with different post systems, and could change the rate of root fracture^{4,8}. Other studies recommend cusp coverage to restore the fracture resistance⁹, because they protect cusps which are not shifted to the outside²¹.

Direct use of composite resins to restore root-filled premolars is deemed to be possible^{13,22}. In the present study, cusp coverage with composite did not increase the fracture resistance of premolars compared with intact teeth. Similar results were found in teeth restored with composite onlays²³. However, cusp coverage was found to significantly strengthen premolars restored with composite onlays⁹. This may be due to the axial direction of the compressive load used in these studies, which would lead to different results when compared with the different load degrees along the long axis of the tooth.

In some study, the evaluation of the effect of fiber post and polyethylene fibers on the fracture resistance of the root-filled maxillary premolars revealed that the fiber post and polyethylene fibers (Ribbond) are better able at distributing the forces along the teeth^{12,24}. Consequently, these materials were introduced to conserve the endodontically-treated teeth.

The results of our study did not show significant differences in fracture resistance between the G2 and G3. The finding that the treatment of restored root canal and defective palatal cusps maxillary premolars with a fiber post exhibited a similar fracture resistance to that of those treated only with composite, is consistent with other studies^{4,25}. This could be due to the fact that the tooth crown structure is too little and the resistance to occlusal forces is weak. On the other hand, it has been suggested that the bonding interface of the restorations could disperse functional stresses, which may reinforce weakened tooth structure. Therefore, it seems that even if the fiber post is not placed, it is possible that the bonding area is big enough and could adequately disperse occlusal forces, rendering the tooth strength to confront the loading forces. However, some studies have reported

that fiber posts provide better fracture resistance in incisors with indirect veneers²⁶. These contrasting result might be due to the type of restorative material, the type and cavity of the teeth, and the direction of the load applied.

The results of our study showed that the fracture strength of the root-filled teeth restored with Ribbond (G4 and G5) was similar to that of the normal teeth, regardless of the use of the fiber posts. In addition, it has been reported that placing a Ribbond on the occlusal surface could increase the fracture resistance of premolars with MOD cavity¹³. Another study demonstrated that anterior teeth restored with a Ribbond inside a root canal achieve a higher resistance strength to fracture¹⁶. It is thought that combined FRC and dentin as a whole, therefore, if a load force is applied to the sample, the fiber would absorb it and reduce the risk of fracture as the intact tooth^{12,16}. During normal function, the cusps of the opposing tooth exert a wedging effect that pushes the B and L cusps apart. The occlusal forces of the opposing cusp are converted into a lateral force within the composite restoration, which pushes against the B and L walls of the cavity. Placing a Ribbond across the cusp B-L splint towards the occlusal forces acts to pull the cusps together when loaded.

The differences between the groups were significant with respect to the failure mode. In the G4 and G5, 80–90% restorable fracture patterns were observed; these results are similar to those of the G1 (80% restorable). The structural continuity of the intact teeth has been reserved, so the loading forces applied do not concentrate in special area¹. This result is consistent with another study, which confirms that polyethylene fiber has a modifying effect on interfacial stresses¹³, and the use of FRC restoration can better protect the remaining tooth structure.

The highest percentage of unfavorable fracture mode (80%) was observed in G3. This might be due to too much root dentin which was cutting, the loading force pass to the weakened root. In addition, the teeth restored using composite with buccal cusp coverage, the composite polymerization shrinkage stresses can impact the failure mode¹. Some studies have also shown that the placement of fiber post produces no improvement in the failure mode of maxillary premolars⁴. In G2, 50% of the fractures were unfavorable, which is higher than those of the intact teeth. When a premolar is restored by full-coverage restorations the stress concentrates on the intercuspatal fissure under loading²⁷. It is plausible that restorations with cuspal coverage facilitate fractures.

The loading force was applied at the central fossa with axial direction of the compressive load of the tooth to simulate occlusal force during this study. However, this may be different to clinical conditions where the extensive occlusal loading applied disperses onto the restorations and, therefore, must be evaluated in future experiments. The different loading conditions such as wedges and balls with various diameters, lead to different results in various studies. Therefore, the relevance of the differences between the various research results depend

on the device and circumstances of the study, rather than the actual values of the fracture loads. Accordingly, the results should be interpreted with caution.

CONCLUSION

Within the limitations of this laboratory experiment, it may be concluded that regardless of the use of the fiber posts, restorations with ribbon fiber-reinforced resin provided superior fracture resistance of premolars with defective palatal cusps and endodontic access cavities when compared with conventional direct restorative techniques. However, additional long-term clinical studies are required to verify these findings.

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